Poisson equation based modeling of DC and AC electroosmosis

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Content

• Introduction

– electroosmosis principle

• Governing equations of electrokinetic flow

- full model
- slip approximation

• Mathematical models

- model of a biosenzor driven by an external DC electric field
- limitations of the slip modeling
- model of electrokinetic flow driven by an AC electric field in a microchannel
- properties of the AC electrokinetic flow
- Conclusion

Electric double layer (EDL)

COMSOL Conference Prague 2006 Page 4 and 2007 Page 4

Electroosmosis induced by DC field

Positive ions accumulates at the charged surfaces

Axially imposed electric field acts on cloud of electric charge and starts fluid movement

Santiago J.G., Stanford microfluidic lab

Governing equations

t

- Mass balances of ionic components (at least 2 equations)
- Navier-Stokes and continuity equations (3 or 4 equations, v_{γ} , v_y , (v_z) , p)

$$
\rho \frac{D\vec{v}}{Dt} = \rho \vec{g} - \nabla P + \rho_{el} \vec{E} + \mu \nabla^2 \vec{v}
$$

$$
\nabla \cdot \vec{v} = 0
$$

 $\frac{\partial c_i}{\partial t} = -\nabla \cdot \vec{J}_i + \sum_j v_{ij} r_j$

 $c_i = -\nabla \cdot \vec{J} + \sum V$

• Poisson equation

$$
\nabla \cdot \nabla \Phi = -\frac{\rho_{el}}{\varepsilon_0 \varepsilon_r}
$$

Slip model of flow

• Simplified Navier-Stokes equation

$$
\rho \frac{\partial \vec{v}}{\partial \lambda} = \rho \vec{g} - \nabla P + \rho_d \vec{E} + \mu \nabla^2 \vec{v}
$$

• Non-zero velocity on microcapillary walls (Helmholtz-Smoluchowski approximation)

$$
\vec{v}\big|_{wall} = -\mu_{eo} \vec{E}\big|_{wall} \qquad \qquad \mu_{eo} = -\frac{\varepsilon_r \varepsilon_0 \phi_{\zeta}}{\eta}
$$

Electroneutrality

$$
\sum_{i} z_{i} c_{i} = 0 \implies \rho_{el} = 0 \implies \nabla \cdot \nabla \Phi = 0
$$

Non-slip model of flow

• Navier-Stokes equation with electric volume force

$$
\rho \frac{\partial \vec{v}}{\partial t} = \rho \vec{g} - \nabla P + \rho_{el} \vec{E} + \mu \nabla^2 \vec{v}
$$

• Zero velocity

$$
\vec{v}\big|_{wall} = 0
$$

• Local deviation from electroneutrality

$$
\sum_{i} z_{i} c_{i} \neq 0 \Rightarrow \rho_{el} \neq 0 \Rightarrow \nabla \cdot \nabla \Phi = -\frac{\rho_{el}}{\varepsilon_{0} \varepsilon_{r}}
$$

Model of a biosenzor driven by an external DC electric field

solution solid ph.

Device consists of 5 compartments DC electric field is applied Ligand + Receptor = Complex DU electric lield is applied
solution solid ph. solid ph. Electric charge attached to walls

Meshing

- 2860 rectangular elements
- non-equidistant
- anisotropic
- the ratio of the larger and the smaller edge of rectangles in interval $10⁰$ - $10⁴$

Short-time elecrokinetic dosing of a ligand in aqueous solution

Formation of the ligand-receptor complex on microchannel wall

Level of saturation of the receptor binding sites

Ligand concentration field

Example of limitation of the slip model – electrolyte concentration

Example of the slip model limitations – ligand-wall (receptor) electrostatic interaction

Effects of the surface electric charge σ_i and ligand charge number z_{4b} on formation of ligand-receptor complex on the microchannel wall

NC is the total number of molecules of the ligandreceptor complex

Principle of AC electroosmosis

M. Mpholo, C.G. Smith, A.B.D. Brown, Sensors and Actuators B Chemical, 92, pp. 262-268, 2003.

Distribution of electric potential along the electrodes (red line) induces tangential movement of the electric charge and thus eddies formation.

Model of electrokinetic flow driven by an AC electric field in a microchannel

Geometry and dimensions of the microchannel $(l_1 = l_5 = h = 10 \text{ µm}, l_2 = 5 \text{ µm}, l_3 = 2 \text{ µm}, l_4 = 3 \text{ µm}.$

Meshing

- 2800 rectangular elements
- non-equidistant
- anisotropic
- the ratio of the larger and the smaller edge of rectangles in interval 10^0 - 2×10^4

Steady periodic regime $A = 1$ V, $f = 1$ kHz

Electric potential distribution **Velocity distribution** (blue $\Delta\Phi$ = -1V, red $\Delta\Phi$ = +1V)

COMSOL Conference Prague 2006 Page 17 No. 2006

Time course of global velocity

Global velocity = the tangential velocity v_x averaged over depth of the microchannel $v \in \langle 0, h \rangle$

Most of the stable periodic regimes (except $f = 1 \times 10^4$ s⁻¹) exhibits changes in flow direction during one period $(1/f) \Rightarrow$ fluid motion in the microchannel has a zigzag character.

However, a continuous flux of electrolyte can be experimentally observed because of high frequency of the zigzag motion $(2f \text{ or } 4f)$.

$$
f_A = 1 \times 10^1 \text{ s}^{-1}, f_B = 1 \times 10^2 \text{ s}^{-1}, f_C = 1 \times 10^3 \text{ s}^{-1}, f_D = 1 \times 10^4 \text{ s}^{-1}, f_E = 1 \times 10^5 \text{ s}^{-1}, f_F = 1 \times 10^6 \text{ s}^{-1}.
$$

Dependence of global velocity on AC frequency, $A = 1$ V

The dependence of the global velocity averaged over one period $(1/f)$ on the applied frequency of AC electric field.

This dependence is in a good qualitative agreement with the experimentally reported one. For the given set of parameters, there are several flow reversals observed in the studied frequency interval. The maximum global velocity is few tents of microns per secondd in the frequency interval $\langle 10^2, 10^4 \rangle$ Hz.

Conclusions

- COMSOL Multiphysics software enables numerical analysis of electro-transport processes based on EDL in macroscopic objects
- Slip approximation is not necessary
- Limitations of the slip approximation in a DC system were identified
- Electroosmosis induced by AC electric field was analyzed in a microfluidic channel
- Dependence of global velocity on AC frequency was computed
- Experimentally observed phenomenon (flow turnover at some frequencies) was proved by numerical analysis
- This phenomenon probably does not rely on chemical and/or electrode reaction