

Cohesive Zone debonding : Evaluation of interfacial adhesion strength of NiTi-PMMA composite and simulation validation

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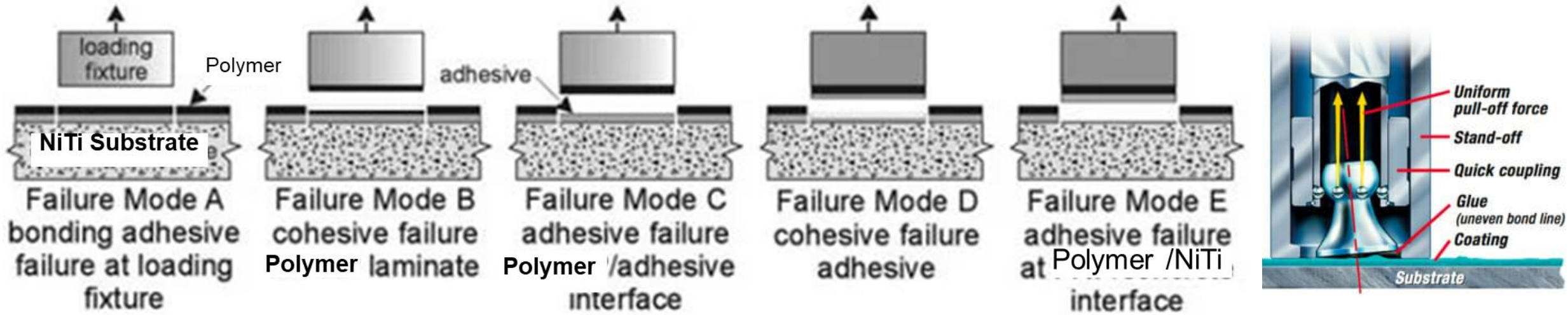
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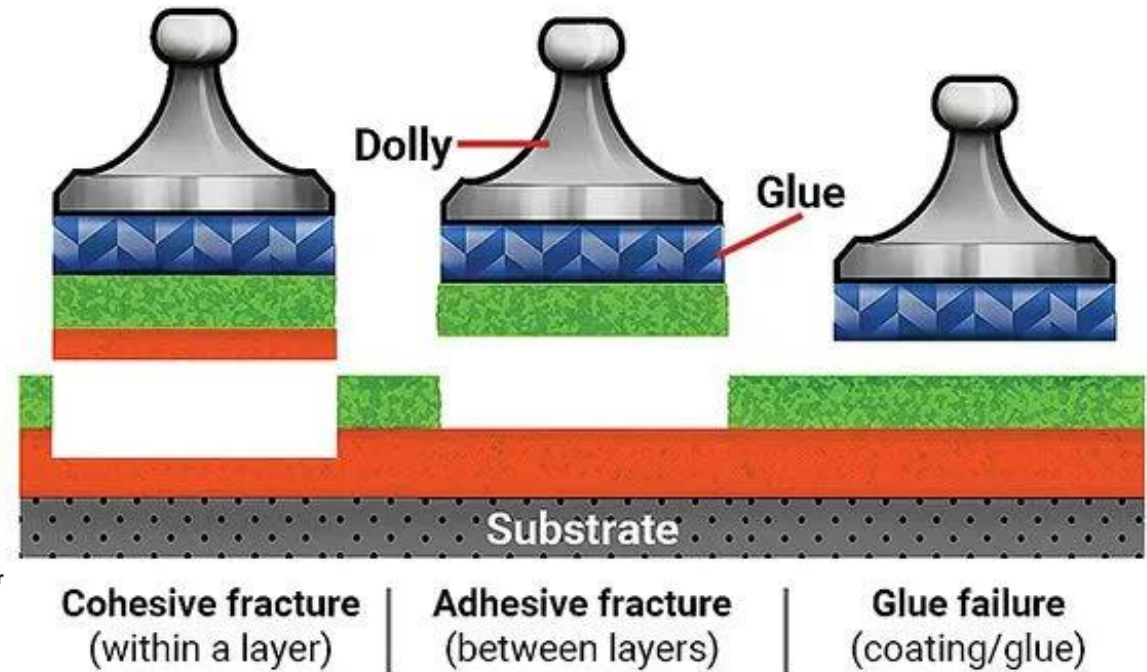
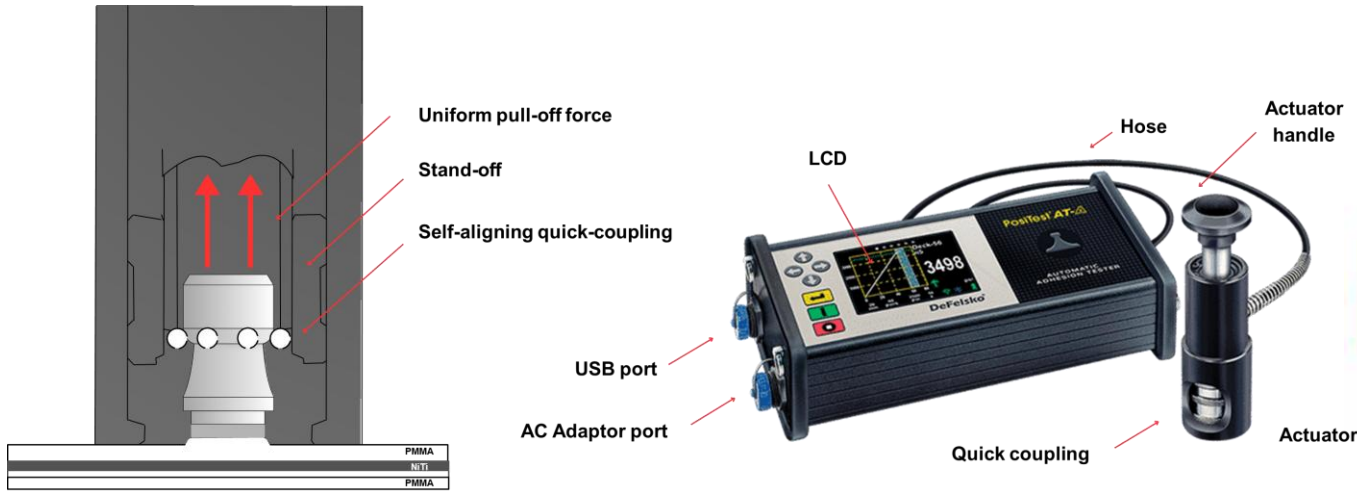
- Introduction about various mode of failure
- Aim and objective
- Experimental analysis
- Internal parameters for simulation
- Model used the interfacial failure
- Results and discussion
- Conclusion

Overview : Mode of failure

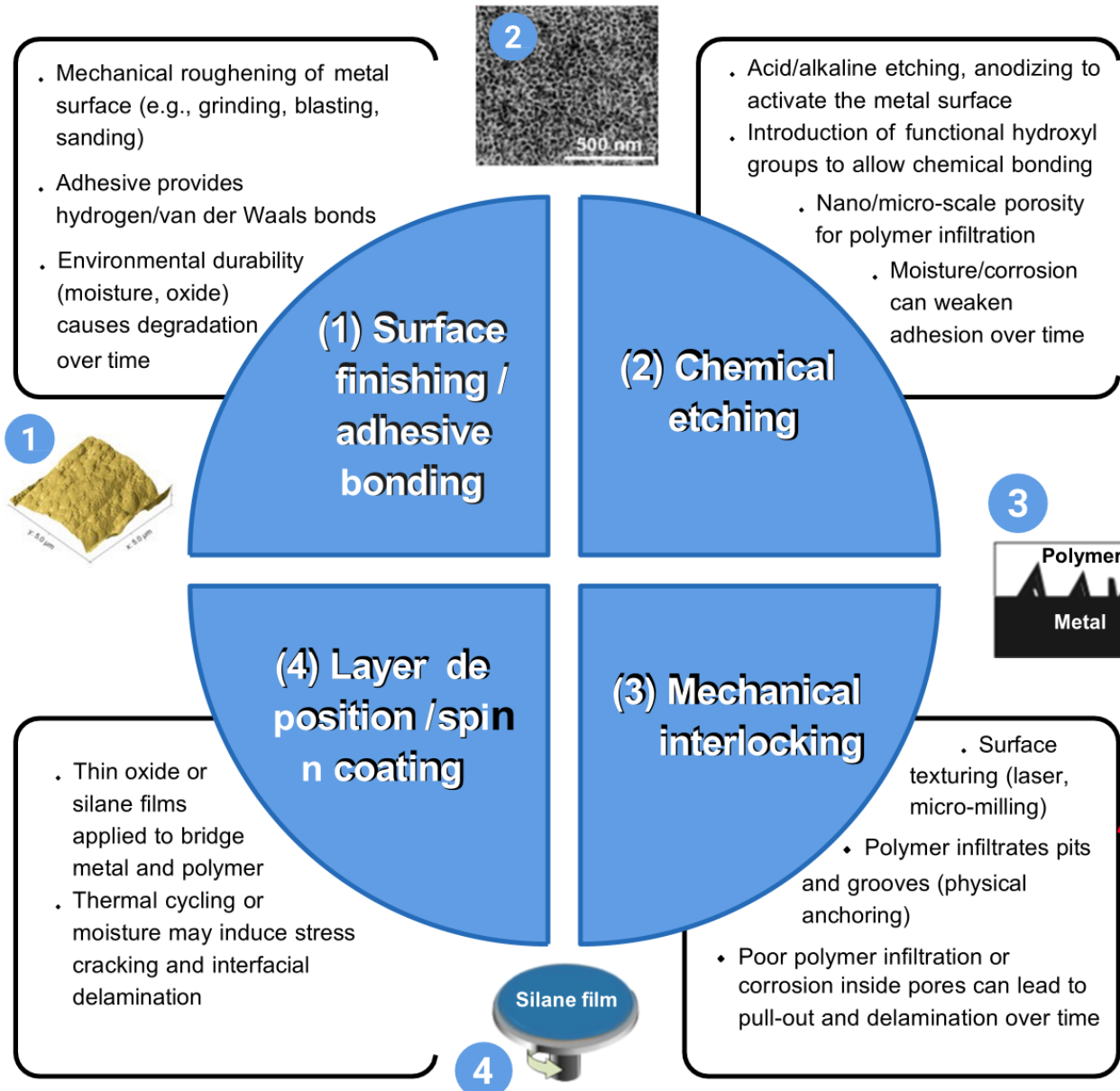


Failure modes for pull-off test (ASTM D7522)

Experimental Set up for pull off test to determine interfacial strength



Aim and objective



Aim:

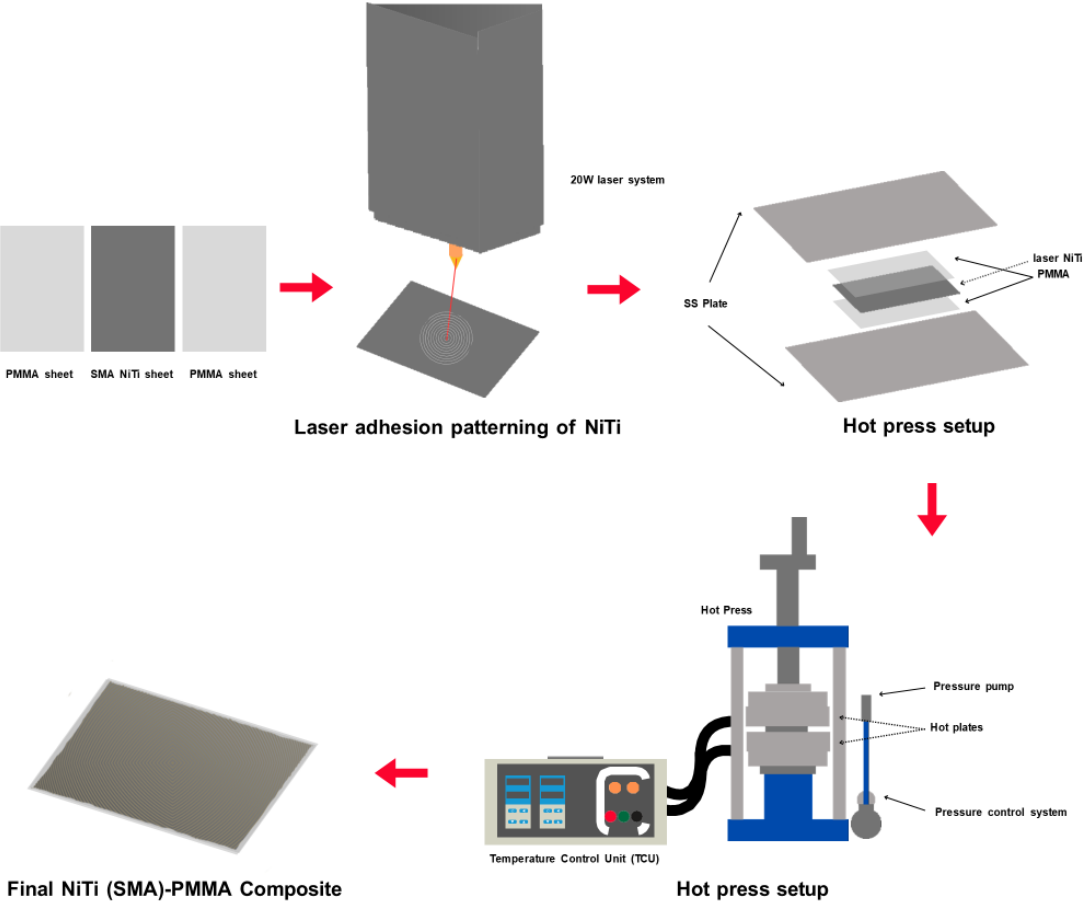
- To establish the interfacial adhesion of the metal-polymer surface in the composite
- To examine the adhesion strength of NiTi-PMMA composite by implementing a pull-off test on the composite surface.

Objectives:

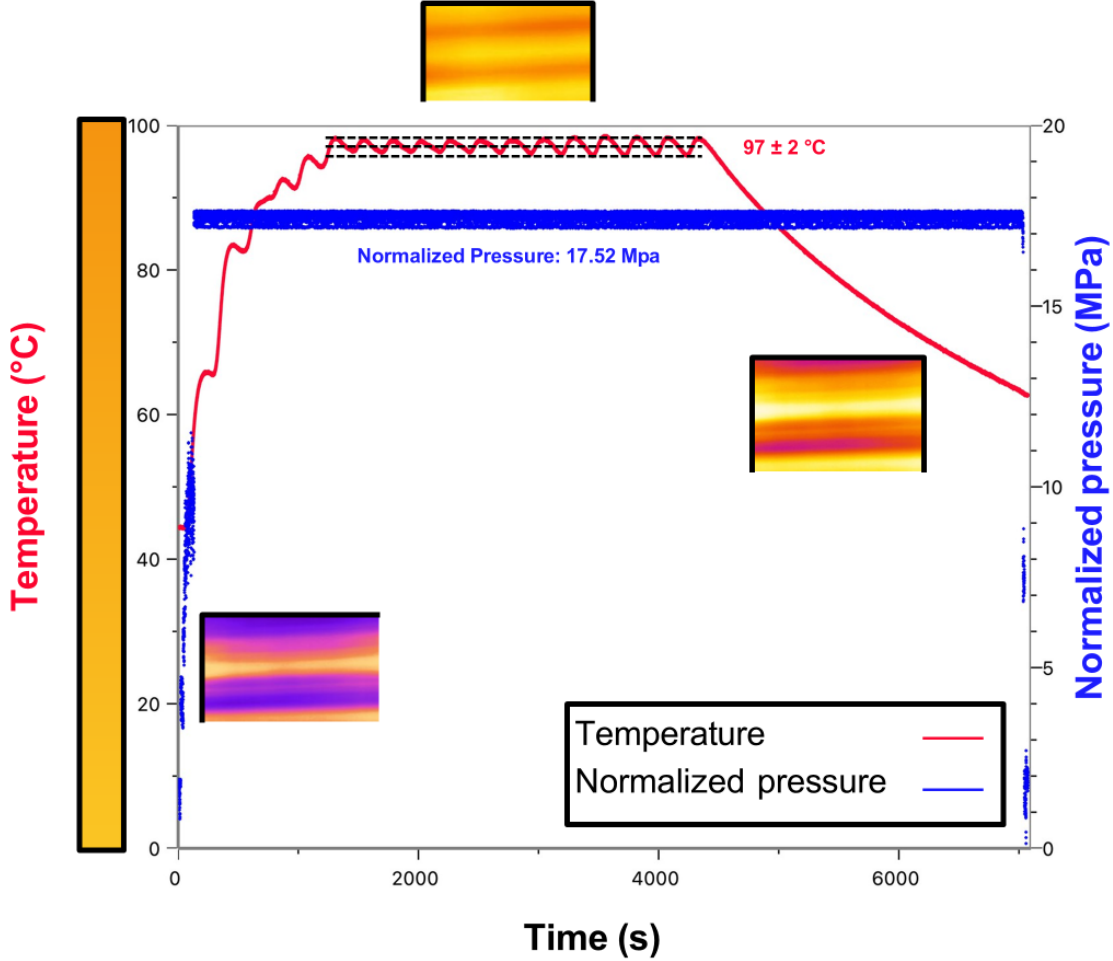
- Mechanical interlocking: create NiTi-PMMA composites for better adhesion with different laser patterns and hot press
- Implement a pull-off test using the PosiTest AT-A automatic adhesion tester
- Compare the maximum strength (MPa) required to pull off PMMA from composite
- Evaluate the mode of failure of the composite

Fabrication of composite by laser surface pattern and hot press system

Fabrication process



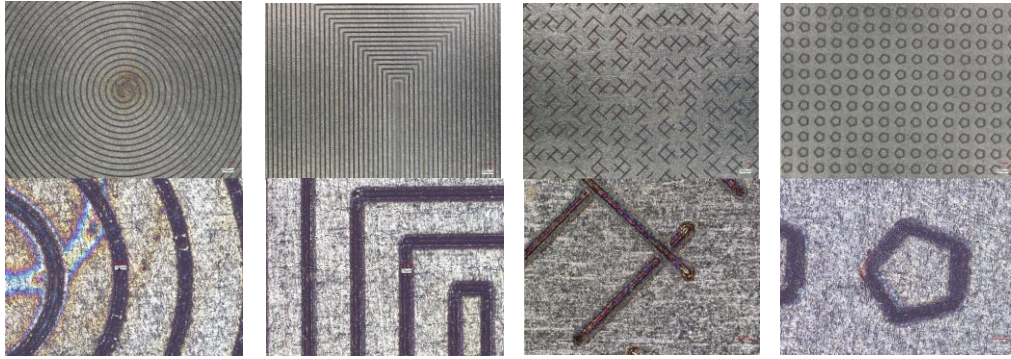
Temperature and pressure profile v.s. time



Various laser surface patterns for adhesion

— 100 μm

NiTi surface with four different laser patterns



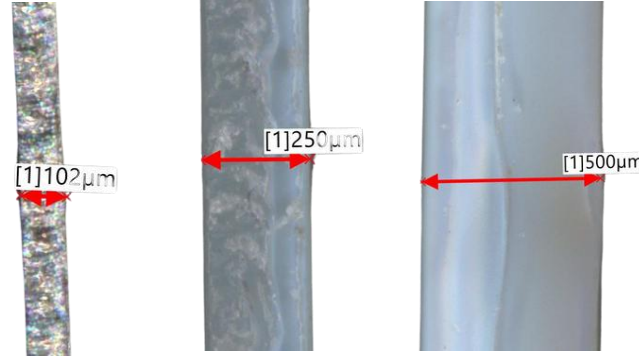
A - Spiral

B - Square

C - Cross

D - Dot

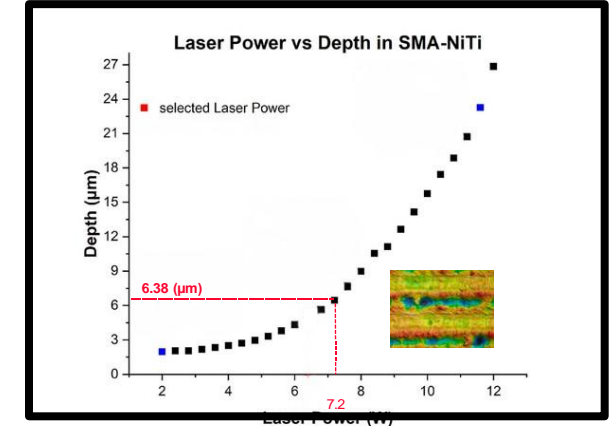
Cross section surface of NiTi, PMMA



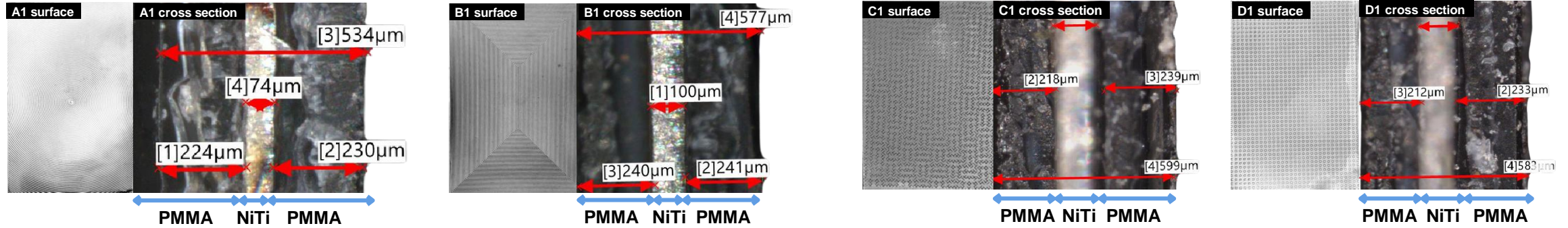
NiTi (100 μm)

1- PMMA (250 μm)

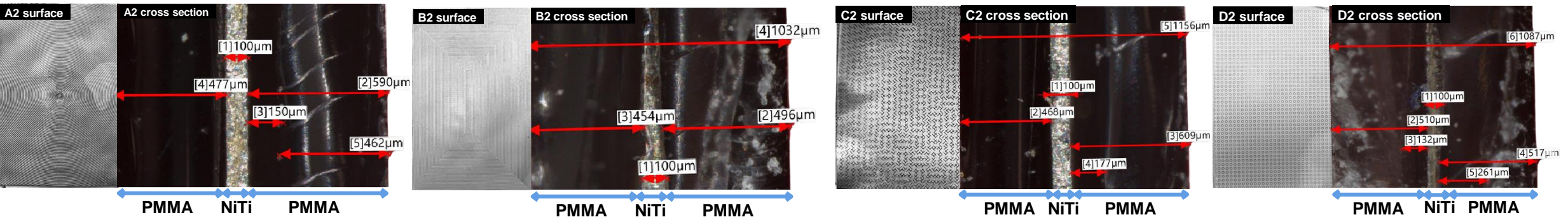
2- PMMA (500 μm)



Surface and cross section of the composite: PMMA (250 μm) - NiTi (100 μm) - PMMA (250 μm), overall thickness of the composite: 600 ± α μm



Surface and cross section of the composite: PMMA (500 μm) - NiTi (100 μm) - PMMA (500 μm), overall thickness of the composite: 1100 ± α μm



Adhesion Pull-off test



Abrasion of dolly and composite surface



Mix epoxy part A and part B



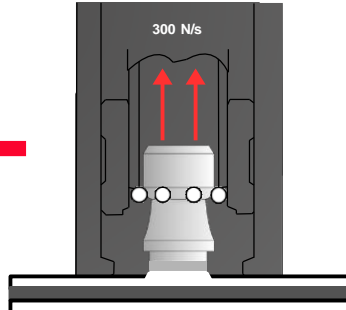
Application on dolly surface



Cure at room temperature for 24~48 hours



Attach actuator onto dolly



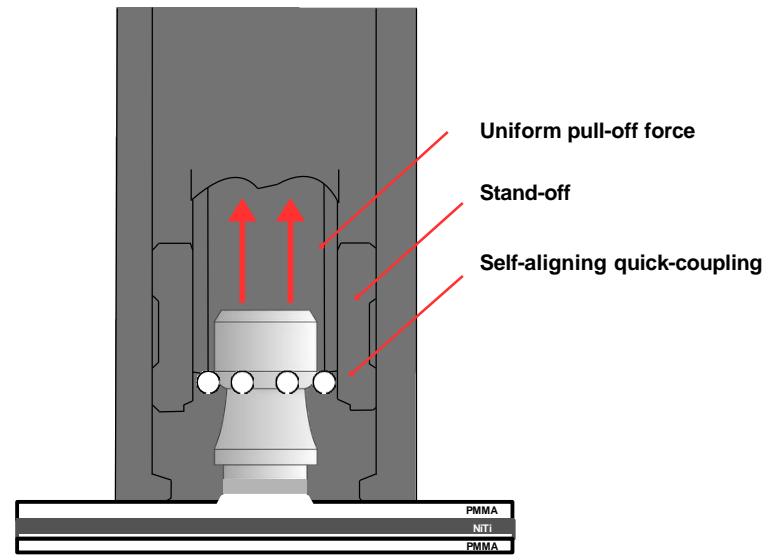
Dolly pulled off



Composite and dolly surface after the pull-off test

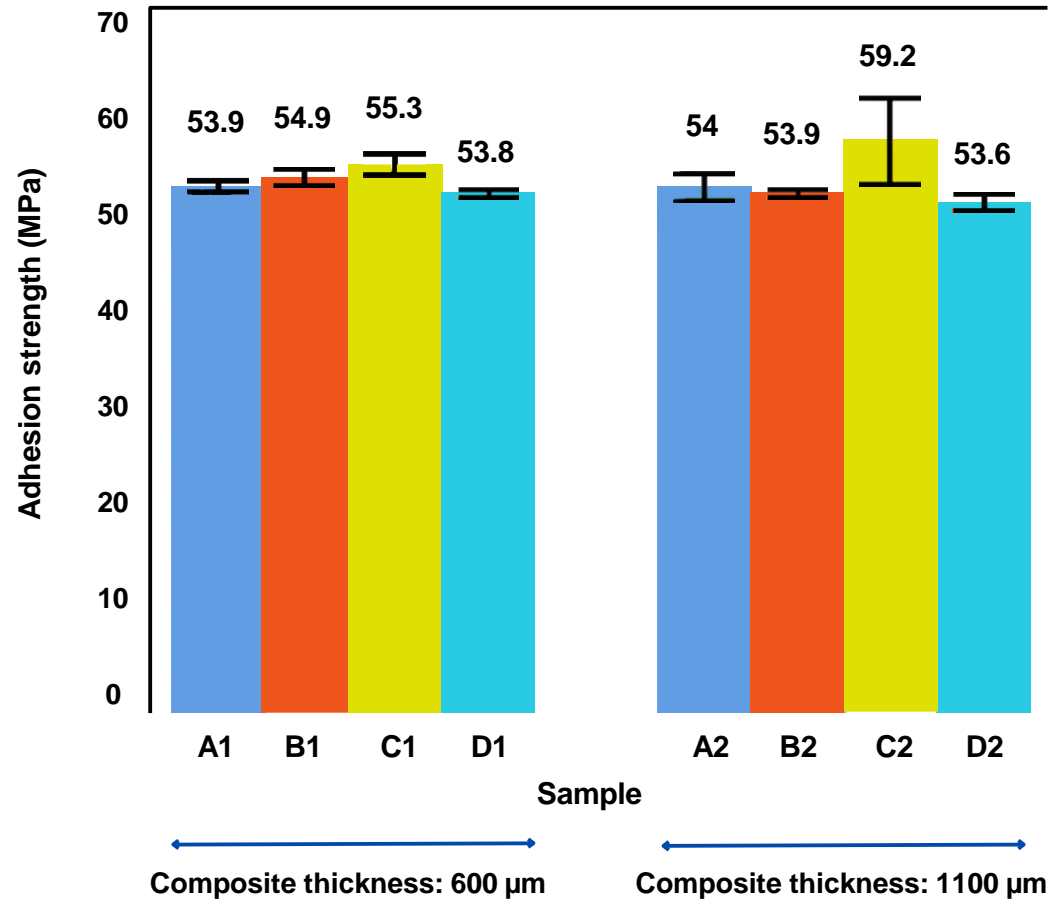
Pull-off parameters

- Maximum force: 7550 N
- Pull rate: 300 N/s
- Dolly: 10 mm

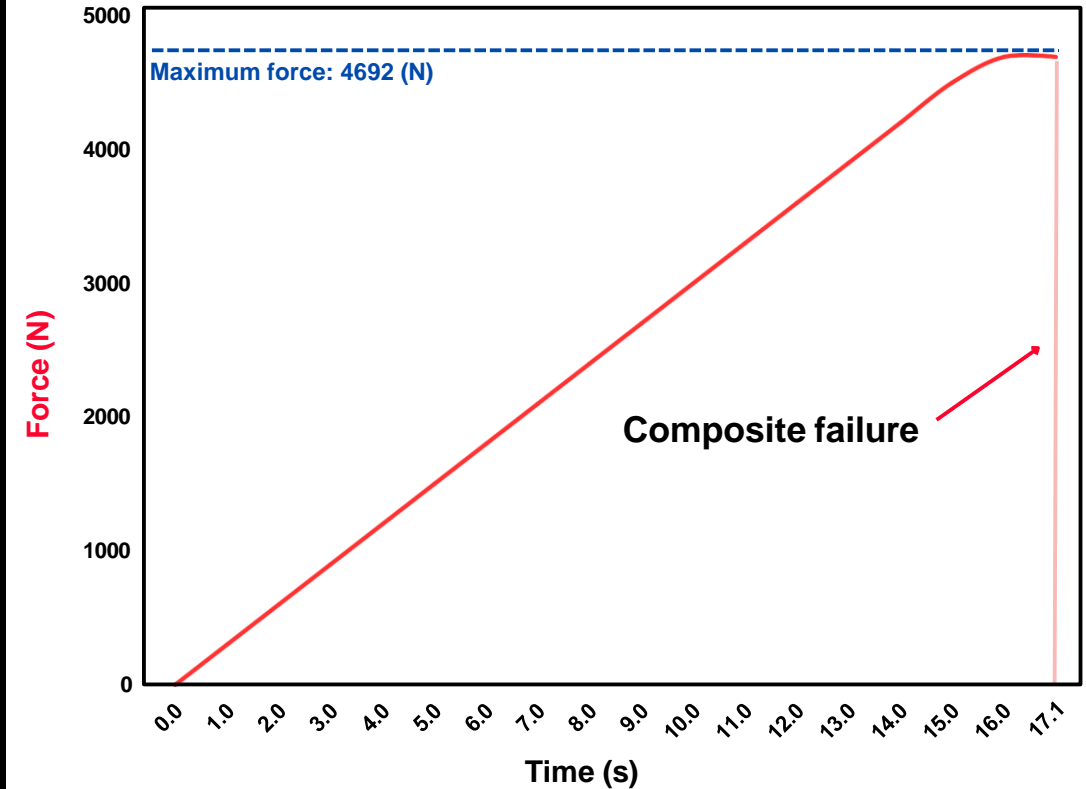


Adhesion strength of composite in pull-off test

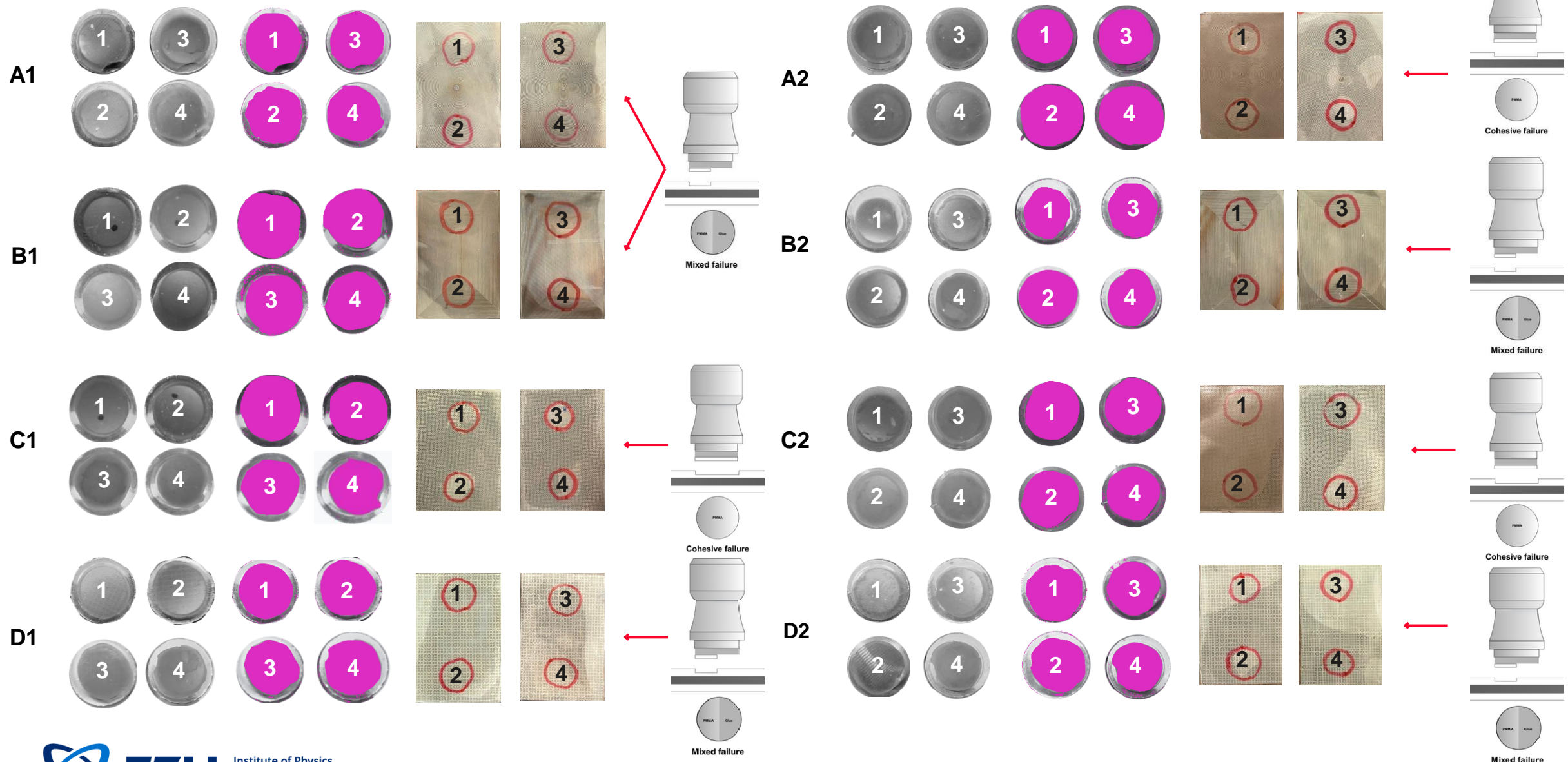
Adhesion strength across samples



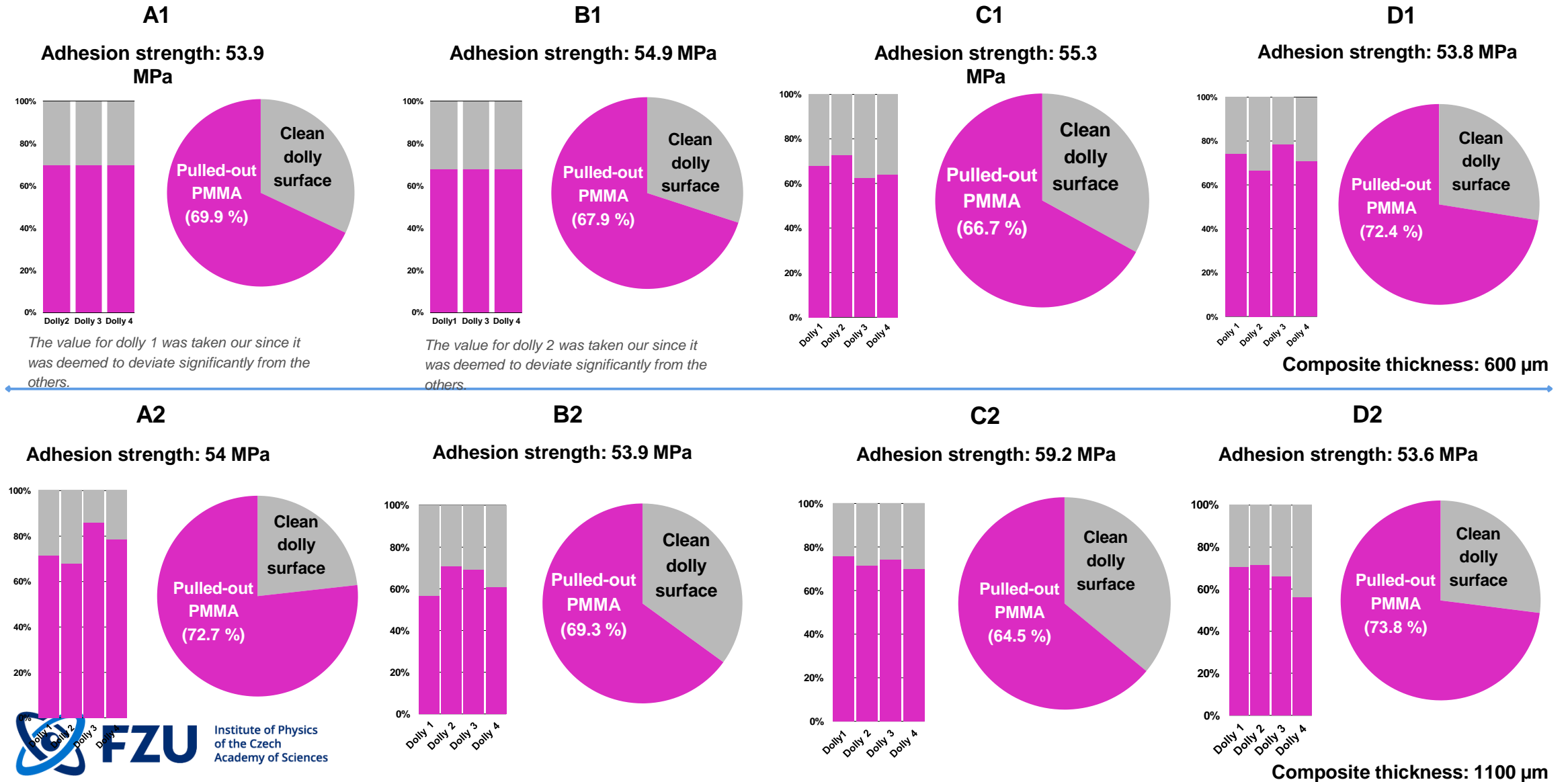
Pull-off test graph (Force (N) v.s. Time (s))



Failure mode: surface observation (both dolly and composite)



Summary of the pull-off test (Adhesion strength and failure mode)



Conclusion

- Sample C2 with the crossed laser pattern and PMMA thickness of 500 μm exhibited the highest maximum pressure of approximately 59.2 MPa.
- Mixed/cohesive failure was observed throughout the pull-off tests, indicating that the adhesion between the NiTi and PMMA interface is stronger than the cohesion within PMMA.
- In failure mode, it is possible to observe that the less pull out of PMMA from dolly surface signify higher interfacial strength.

Mixed-Mode Debonding of a Laminated Composite

Interfacial failure by delamination or debonding can be simulated with a Cohesive Zone Model (CZM). This example shows the implementation of a CZM with a bilinear traction-separation law. It is used to predict the mixed-mode softening onset and delamination propagation in a composite material.

| | | | |
|--------|---|-----------------------|---|
| lb | 102[mm] | 0.102 m | Length |
| wb | 25.4[mm] | 0.0254 m | Width |
| hb | 2*1.56[mm] | 0.00312 m | Thickness |
| cl | 34.1[mm] | 0.0341 m | Initial crack length |
| pn | 1e6[N/mm ³] | 1E15 N/m ³ | Penalty stiffness |
| sigmat | 65[MPa] | 8E7 Pa | Normal tensile strength |
| sigmas | 50[MPa] | 1E8 Pa | Shear strength |
| Gct | 0.969[kJ/m ²] | 969 J/m ² | Critical energy release rate, tension |
| Gcs | 1.719[kJ/m ²] | 1719 J/m ² | Critical energy release rate, shear |
| alpha | 2.284 | 2.284 | Exponent of the Benzeggagh and Kenane (B-K) criterion |
| disp | 0 | 0 | Displacement parameter |
| mm | 0.5 | 0.5 | Mode mixity ratio |
| ll | $lb/2*(0.5*\sqrt{3*(1-mm)/mm}+1)/(3-0.5*\sqrt{3*(1-mm)/mm})$ | | 0.044596 m Lever length |
| lr | $8*((6*mm+\sqrt{3*mm*(1-mm)})/(3+9*mm+8*\sqrt{3*mm*(1-mm)}))$ | | 2.1436 Load ratio middle/cracked edge |

Transversely isotropic

Density 2050 kg/m³

Young's modulus {30, 3.1} GPa

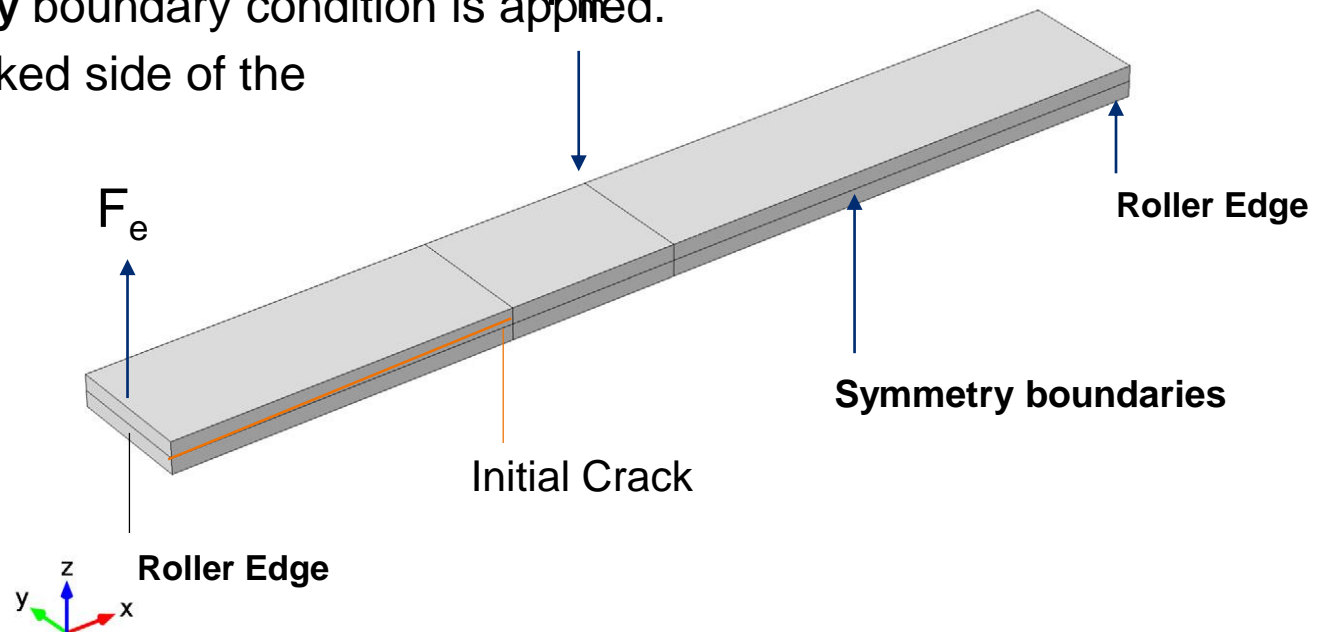
Poisson's ratio {0.42, 0.35} 1

Shear modulus 20 [GPa] N/m²

It consists of a beam cracked along a ply interface halfway through its thickness. The initial crack length is a . The beam

is supported at the outermost bottom edges. A mixed-mode bending load is produced as the result of forces applied to the top edges at the cracked end and at the center of the beam. Because of the symmetry, only half of the beam is modeled and a **Symmetry** boundary condition is applied.

A pulling force F_e is acting on the cracked side of the beam. At the center, a force F_m pushes down.



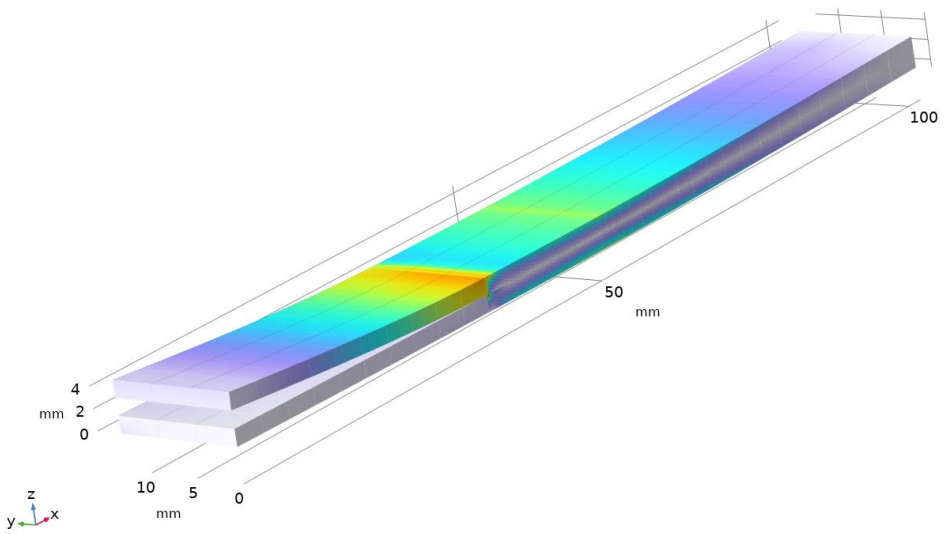
Interfacial failure by delamination or debonding is one of the main failure modes of laminate structures. Such failures can be simulated with a cohesive zone model (CZM). A key ingredient of a cohesive zone model is a traction-separation law that describes the softening in the cohesive zone near the delamination tip. This example shows how to model debonding using the decohesion model in COMSOL Multiphysics. The capabilities of the CZM to predict mixed-mode softening and delamination propagation are demonstrated in a model of the mixed-mode bending of a composite.

The screenshot displays the COMSOL Multiphysics interface for a model titled "cohesive_zone_debonding.mph". The software is running on a Windows operating system, as indicated by the taskbar. The interface is divided into several main sections:

- Model Builder:** Shows the hierarchical structure of the model. Key components include:
 - Global Definitions: Parameters 1.
 - Materials: PMMA/NiTi/PMMA sandwich composite (mat1), Basic (def), Transversely isotropic (Transversely isotropic).
 - Component 1 (comp1):
 - Definitions: Load Point Variables, Integration Edge (intop1), Integration Center (intop2), Boundary System 1 (sys1).
 - View 1.
 - Geometry 1: Block 1 (blk1), Block 2 (blk2), Form Union (fin).
 - Materials: Material Link 1 (matlink1), Solid Mechanics (solid).
 - Linear Elastic Material 1: Free 1, Initial Values 1, Interior Contact 1, Auxiliary Slit 1, Symmetry 1, Load on Cracked Edge (Fe), Load on Middle Edge (Fm), Prescribed Displacement 1, Prescribed Displacement 2, Global Equations 1 (ODE1).
 - Mesh 1.
 - Study 1: Step 1: Stationary, Solver Configurations, Solution 1 (sol1) with Compile Equations: Stationary, Dependent Variables 1, and Stationary Solver 1.
- Settings:** Shows the properties for the selected "Linear Elastic Material 1".
 - Label: Linear Elastic Material 1.
 - Domain Selection: Selection: All domains.
 - Coordinate System Selection: Global coordinate system.
 - Linear Elastic Material:
 - Material symmetry: Orthotropic.
 - Material data ordering: Standard (11, 22, 33, 12, 23, 13).
 - Young's modulus: E (From material).
 - Poisson's ratio: ν (From material).
 - Shear modulus: G (From material).
 - Density: ρ (From material).
- Graphics:** Displays a 3D perspective view of the composite beam. The beam is oriented along the x-axis, with a length of 100 mm, a width of 50 mm, and a thickness of 3 mm. A coordinate system (x, y, z) is shown at the origin. Two forces are applied: F_e (upward) and F_m (downward). The beam is meshed with a fine grid. The status bar at the bottom indicates a memory usage of 1.75 GB | 1.87 GB.

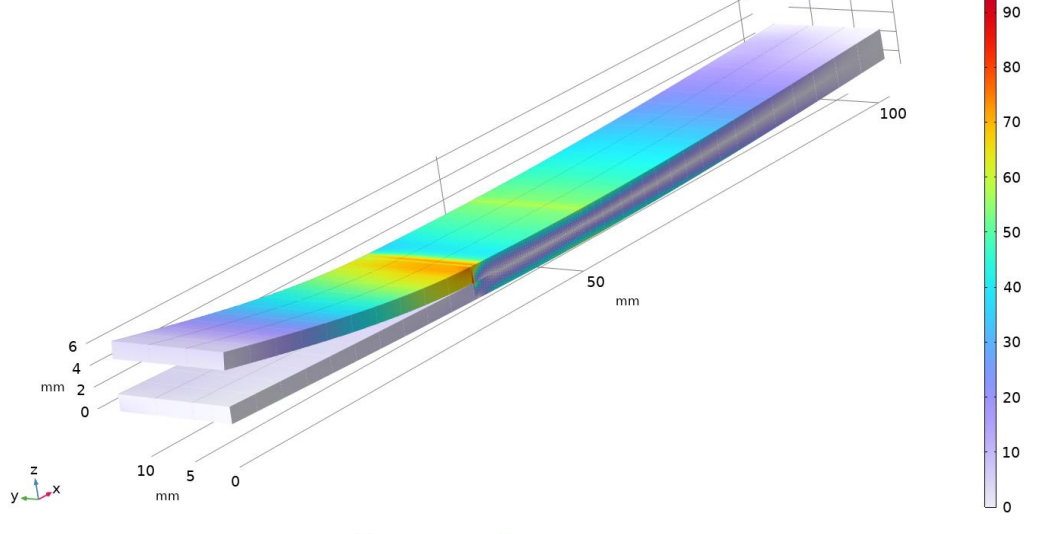
disp(9)=0.0016

Volume: von Mises stress (MPa)



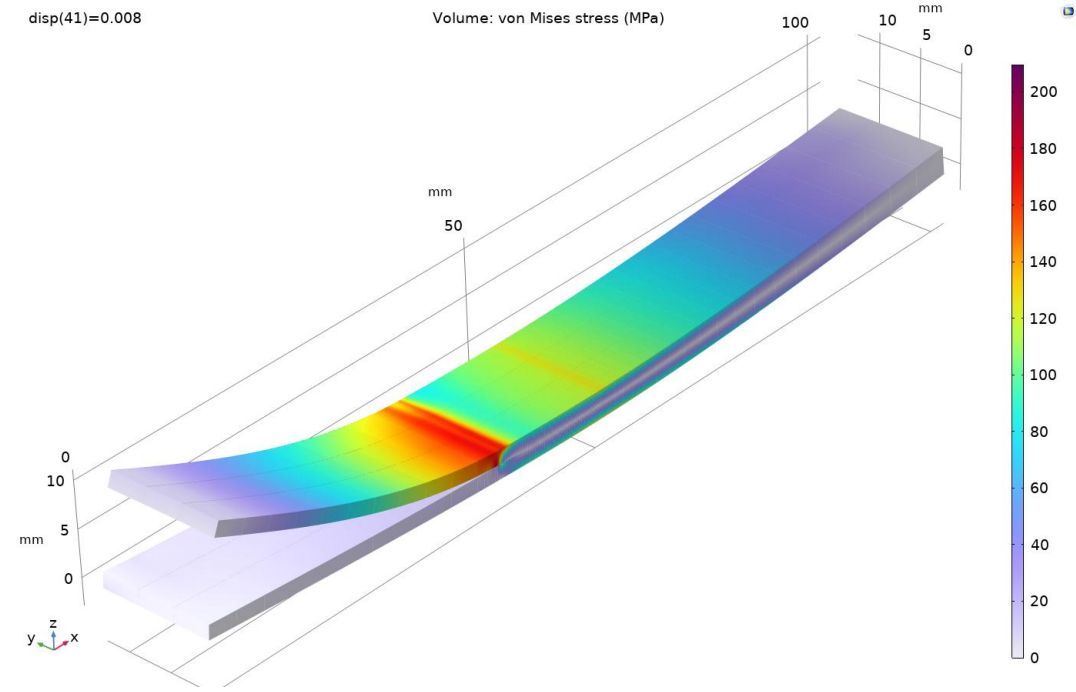
disp(17)=0.0032

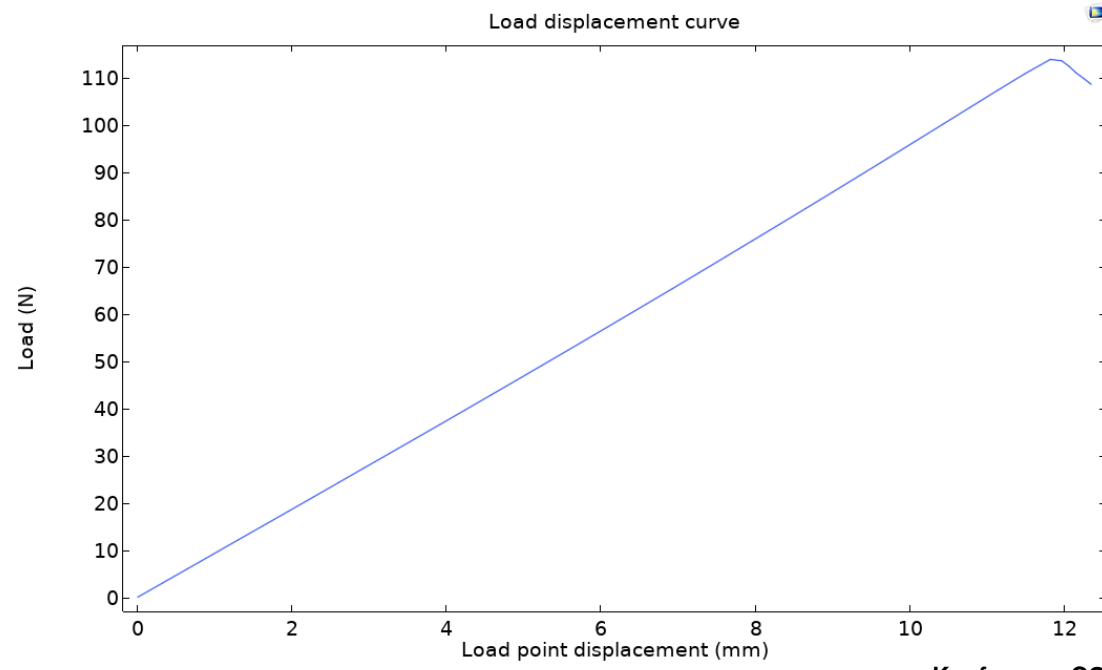
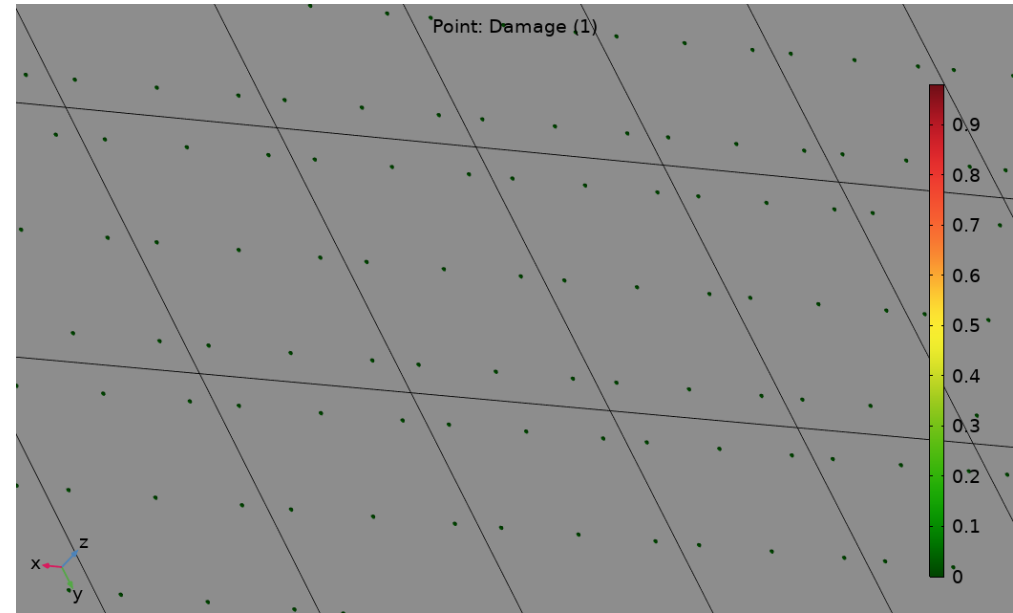
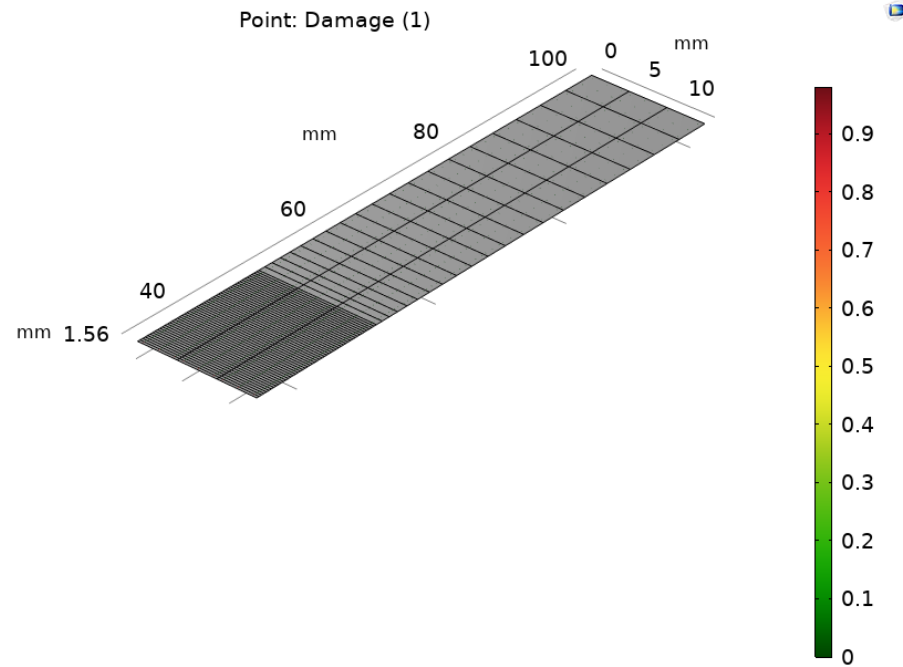
Volume: von Mises stress (MPa)



disp(41)=0.008

Volume: von Mises stress (MPa)





The maximum load that the beam with the initial crack can carry is exceeded and delamination occurs. After exceeding a peak load, the load decreases until the displacement reaches around 11 mm. This point approximately corresponds to when the crack reaches the center of the specimen. Thereafter, the load starts to increase again, but with a much lower stiffness than before delamination.

To implement a cohesive zone model in COMSOL Multiphysics, add an **Adhesion** subnode with a **Decohesion** subnode to the **Interior Contact** node

the simulation must be displacement controlled. This is obtained by using a global equation, in which the distributed load is controlled by the sweep parameter, which is the displacement at the free edge.

Since no large relative deformations of the laminates are expected, the **Interior Contact** node is utilized to model the behavior between laminates.

Thank you

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